

Blind self-interference cancelation for amplify and forward relaying

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In this paper we introduce a self-interference (SI) cancelation technique for amplify and forward relays. Relays are used to help forward signals between a transmitter and a receiver. This helps increase the signal coverage and reduce the required transmitted signal power. One issue that faces relays communications is the SI problem where an unwanted leaked signal from the relay's output will contaminate the new signal received from the transmitter at the relay's input. A solution is proposed in this paper to cancel this SI which is based upon using the constant modulus adaptive algorithm. This is performed blindly at the relay without the need of any training, a priori knowledge of the SI channel or any other channel weight estimates nor the need of multiple antennas. Simulation results are provided to verify the performance of the proposed method.

1 Introduction

Relays are used in wireless communications to decrease the required transmission power between the transmitter and the receiver or to expand the coverage area or a combination of both [3]. Two types of relays are used, amplify and forward (AF) and decode and forward (DF) [2]. The AF is simpler and its function is to amplify the signal it receives and sends it to the destination. Whereas, the DF decodes the signal first then it re-sends it to the destination. One problem that faces these relays is the fact that the signal sent from its output is leaked to its input due to the imperfect antennas isolation between the relay's output and input. This self-interference (SI) will cause degradation in the relay's system performance.

Many of the discussed relays in the literature assume a priori knowledge of the SI channel such as in [1, 4, 5, 8, 9]. Also, antenna arrays in a multiple-input-multiple-output (MIMO) scheme are required by many methods to perform the SI cancelation [5-9]. The authors in [4] propose an optimised gain control scheme to maximise the overall signal-to-interference-noise-ratio (SINR). The methods in [5] and [9] propose spatial-based solution

to this problem. The method in [8] uses precoding techniques to minimise the SI.

A solution is proposed in this paper to cancel this SI which is based upon using the constant modulus adaptive algorithm. The process is performed blindly at the relay without the need of any training nor there is a need for a priori knowledge of the SI channel or any other channel weight estimates. Also, unlike some of the other SI mitigation algorithms, the proposed method does not require multiple antennas to perform the SI cancelation. So, the single-input-single-output (SISO) case is considered in this paper. Still the method can be extended to the MIMO case. This SI cancelation method is named the constant-modulus-based-SI-cancelation (CM-SI) method.

The rest of the paper is organised as follows: Section II presents the system model. Section III explains the CM-SI method. Sections IV presents the simulation results for the CM-SI method. Followed by conclusions in Section V.

2 System Model

Let us consider a SISO relay case. Let $y_r(t)$ be the received signal at the relay at time t . This signal can be modeled as

$$y_r(t) = \alpha x_s(t) + n_r(t) \quad (1)$$

where $x_s(t)$ is the QPSK signal transmitted by the source, α is an amplifying gain for the transmitted signal, α is the source-relay channel weight and $n_r(t)$ is a circularly symmetric additive white Gaussian noise (CAWGN) of zero mean and variance σ_n^2 .

The relay's transmitted signal is denoted by $x_r(t)$. So, the SI signal can be modeled as

$$x_r(t) = \beta y_r(t) + n_{si}(t) \quad (2)$$

where β is the channel weight for the SI and $n_{si}(t)$ is CAWGN of zero mean and variance σ_{si}^2 .

Also, at the relay, the transmitted signal $x_r(t)$ is a function of its input signal $y_r(t)$, i.e.,

$$x_r(t) = f(y_r(t)) \quad (3)$$

where $y_r(t)$ is the total signal received at the relay's input (this signal is composed of the signal received from the source added with the SI signal coming the relay's output), i.e.,

The function $f(\cdot)$ depends on the type of relay used (e.g. AF or DF). In this paper the AF relay is

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assumed, and assuming that there is a delay in the relay and no significant delay introduced by the SI channel (recall that the relay size is small and its output and input are close to each other), so

where α is the amplifying gain produced by the relay and τ is the delay caused by the relay. Without any loss of generality we will assume that τ is equal to one time index, i.e., $\tau = 1$, so that

As a result, the signal received at the receiver is given by

where β is the relay-destination channel weight and n is CAWGN of zero mean and variance σ^2

3 CM-SI

The CM-SI is a method proposed in this paper to cancel the SI channel (h_{sr}) blindly at the relay. The CM-SI is based upon using a feedback single tapped filter connecting the relay's output to its input. Let this filter output be modeled as

where w is the filter's weight. This filter output will be subtracted from the received signal at the relay's input given in (3) as follows

where

which is CAWGN of zero mean and variance σ^2 . Ideally w should equal h_{sr} thus canceling the SI effect.

Since we are not assuming the knowledge of h_{sr} we propose using the constant modulus adaptive filter to get w . If the SI cancelation is successful, the total received signal at the relay will ideally have a magnitude $|h_{rd}|$. For the sake of algorithm derivation let us consider the noise free version of y_r (which we denote as \tilde{y}_r), i.e.,

Thus,

$$y_r = \alpha h_{sr} x + \alpha h_{rd} x + n$$

$$(4) \quad y_r = \alpha h_{sr} x + \alpha h_{rd} x + n$$

$$(5) \quad \text{Now use (9) to replace the linear term } \alpha h_{sr} x \text{ by}$$

$$(5) \quad \alpha \hat{h}_{sr} x + \alpha h_{rd} x + n$$

$$(6) \quad \text{This yields}$$

$$(6) \quad \alpha \hat{h}_{sr} x + \alpha h_{rd} x + n$$

$$(7) \quad \text{Now we update } \hat{h}_{sr} \text{ using the constant modulus update equation}$$

$$(7) \quad \hat{h}_{sr} = \mu (|h_{sr}|^2 - |\hat{h}_{sr}|^2) \hat{h}_{sr} + \alpha h_{sr} x$$

$$(8) \quad \text{where } \mu \text{ is the update factor and } \alpha \text{ (recall that we are}$$

$$(8) \quad \text{assuming that } h_{sr} \text{ has a Rayleigh distribution, but it is constant over one detection period). So, (12) becomes}$$

$$(9) \quad \hat{h}_{sr} = \mu (|h_{sr}|^2 - |\hat{h}_{sr}|^2) \hat{h}_{sr} + \alpha h_{sr} x$$

$$(10) \quad \hat{h}_{sr} = \mu (|h_{sr}|^2 - |\hat{h}_{sr}|^2) \hat{h}_{sr} + \alpha h_{sr} x$$

$$(11) \quad \hat{h}_{sr} = \mu (|h_{sr}|^2 - |\hat{h}_{sr}|^2) \hat{h}_{sr} + \alpha h_{sr} x$$

$$(12) \quad \hat{h}_{sr} = \mu (|h_{sr}|^2 - |\hat{h}_{sr}|^2) \hat{h}_{sr} + \alpha h_{sr} x$$

$$(13) \quad \hat{h}_{sr} = \mu (|h_{sr}|^2 - |\hat{h}_{sr}|^2) \hat{h}_{sr} + \alpha h_{sr} x$$

$$(14) \quad \text{Notice that the first term in (11) is a constant. Also, when the adaptive filter reaches steady state, it is reasonable to assume that } \hat{h}_{sr} \text{ is small enough, then the second term can be neglected. Thus, it follows that}$$

$$(15) \quad \hat{h}_{sr} = \mu (|h_{sr}|^2 - |\hat{h}_{sr}|^2) \hat{h}_{sr} + \alpha h_{sr} x$$

$$(16) \quad \text{and the update equation (13) now reads}$$

$$(17) \quad \hat{h}_{sr} = \mu (|h_{sr}|^2 - |\hat{h}_{sr}|^2) \hat{h}_{sr} + \alpha h_{sr} x$$

$$(18) \quad \text{Since we are assuming that } \hat{h}_{sr} \text{ and } \alpha \text{ are unknowns at the relay then } \alpha \hat{h}_{sr} \text{ is also unknown. So, we suggest to obtain } \alpha \hat{h}_{sr} \text{ adaptively using the following constant modulus update equation that runs together with (15)}$$

$$(19) \quad \alpha \hat{h}_{sr} = \mu (|\alpha \hat{h}_{sr}|^2 - |\alpha \hat{h}_{sr}|^2) \alpha \hat{h}_{sr} + \alpha h_{sr} x$$

$$(20) \quad \text{where } \alpha \hat{h}_{sr} \text{ is the estimated value for } \alpha \hat{h}_{sr} \text{ at time index } n \text{. Evaluating the gradient part in (16) and}$$

replacing \hat{h}_{sr} with \hat{h}_{sr}^* yields

$$\hat{h}_{sr}^* = \frac{\hat{h}_{sr}}{\|\hat{h}_{sr}\|} \quad (17)$$

Thus, the CM-SI method consists of the following update equations

$$\hat{h}_{sr}^* = \frac{\hat{h}_{sr}}{\|\hat{h}_{sr}\|} \quad (18)$$

$$\hat{h}_{sr}^* = \frac{\hat{h}_{sr}}{\|\hat{h}_{sr}\|} \quad (19)$$

Note that the CM-SI method runs without the need for any training or a priori knowledge of the SI channel or any other channel weight estimates and without the requirement of multiple antennas at the relay.

4 Simulation Results

In this section, simulation results are provided to verify the performance of CM-SI. Without any loss of generality, the noise variances for the source-relay and the SI channels are assumed to be equal, i.e., $\sigma_{sr}^2 = \sigma_{si}^2$. Thus, the variance

is defined as σ^2 . The signal-to-noise-ratio is defined as $\text{SNR} = \frac{P_s}{\sigma^2}$. The gain α and the factor β are set to be equal to 1 and 1, respectively. Also, the initial value of \hat{h}_{sr} is set to

where θ is a random variable. Assuming that the channels are fading, then \hat{h}_{sr} and \hat{h}_{sr}^* are changing and their changes are modeled as follows

$$\hat{h}_{sr} = \hat{h}_{sr} + \delta \hat{h}_{sr} \quad (19)$$

and

$$\hat{h}_{sr}^* = \hat{h}_{sr}^* + \delta \hat{h}_{sr}^* \quad (20)$$

where δ and δ^* is taken to be random drawn from a zero mean circular additive white Gaussian distribution and variance 1. The parameters α with β are CAWGN of zero mean and variances α^2 and 1, respectively. Also, α and β are factors chosen from the period τ to indicate how close the parameters initialisations are to their true value. Smaller (large) values for α or β correspond to close (far) initialisation. Note that α and β is constant, thus initialisation for \hat{h}_{sr} will correspond to initialisation for \hat{h}_{sr}^*

Also, assume that \hat{h}_{sr} and \hat{h}_{sr}^* initially equals \hat{h}_{sr} and \hat{h}_{sr}^* , respectively. Now, because of the channels changing nature due to fading, \hat{h}_{sr} and \hat{h}_{sr}^* have to track these changes.

Fig. 1 shows the learning curves averaged over N ensembles for \hat{h}_{sr} using the CM-SI method for different values of α with β fixed at 1. Clearly, \hat{h}_{sr} approaches the value \hat{h}_{sr} successfully. Also, as expected, the performance is enhanced as α increases. Fig. 2 shows the bit-error-rate (BER) (evaluated at the relay after the cancelation stage) for the CM-SI method over different values of SNRs and over different values of α with β fixed at 1. Clearly, the results shown in Fig. 2 indicate the CM-SI method succeeds in canceling the SI effect.

5 Conclusion

In this paper we introduced a SI cancelation technique for AF relays. The proposed CM-SI algorithm is based upon the constant modulus adaptive algorithm. The method does not require any training, any a priori knowledge of the SI channel or any other channel weight estimates nor does it require multiple antennas to perform the SI cancelation. Simulation results were presented to illustrate the proposed method performance.

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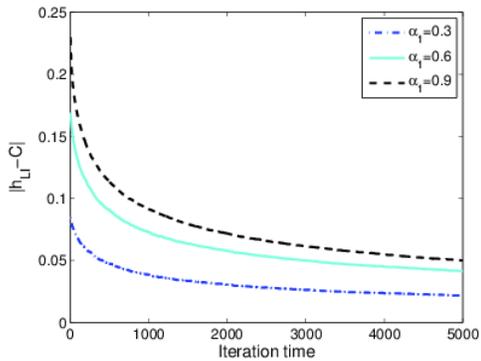


Figure 1: Learning curve for 

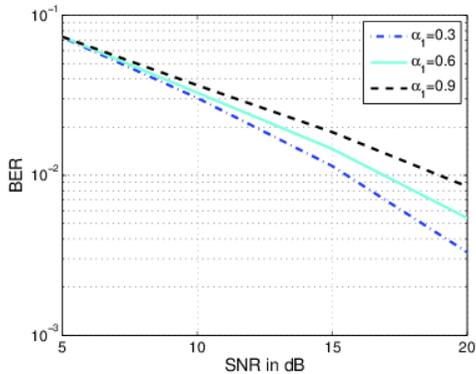


Figure 2: BER vs. SNR.