

Stability of Natural Slopes and Embankments Underlain By Weak Clays

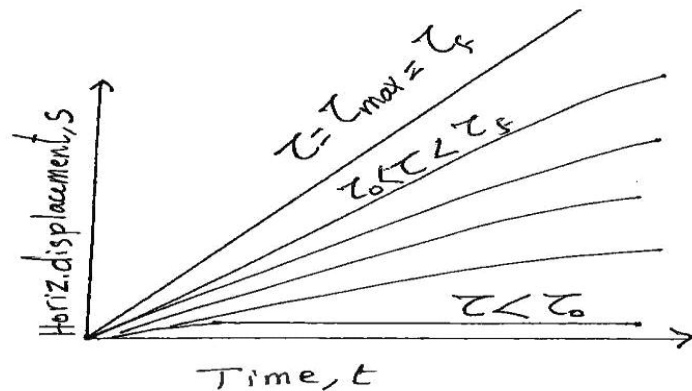
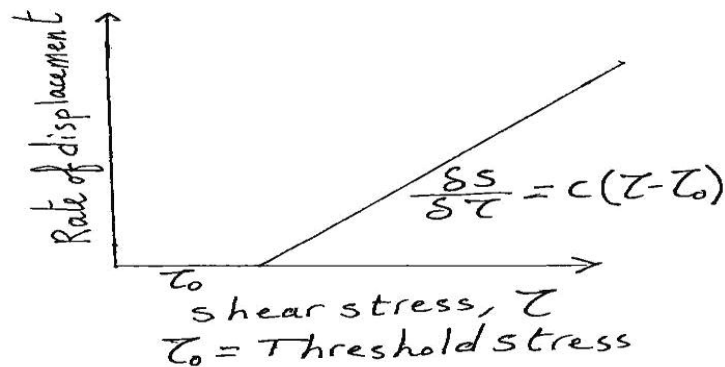
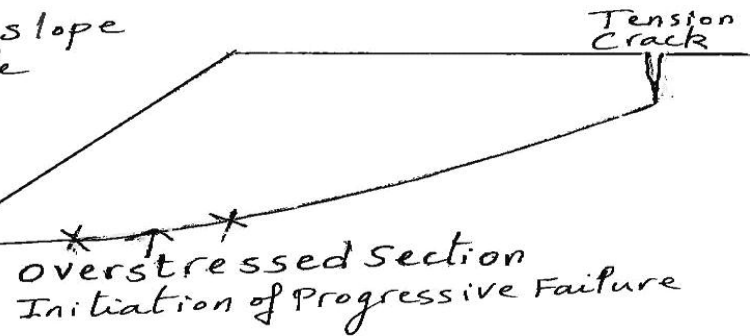
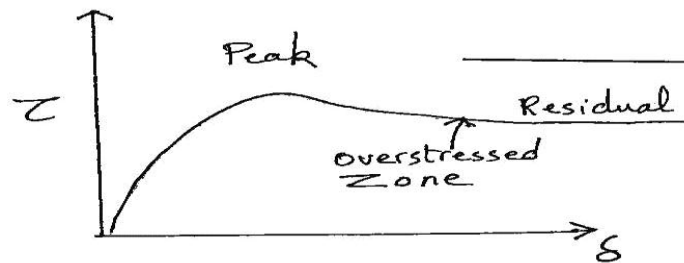
Prof. Dr. Yousef M. Masannat

Stability of Natural Slopes and Embankments

Underlain by Weak Clays

Creep displacement and progressive failure

To avoid progressive failure in cohesive soils with $\phi_u = 0^\circ$, $F.S_{min} = 1.44$ for slope angle of 16° and 1.49 for slope angle of 34°



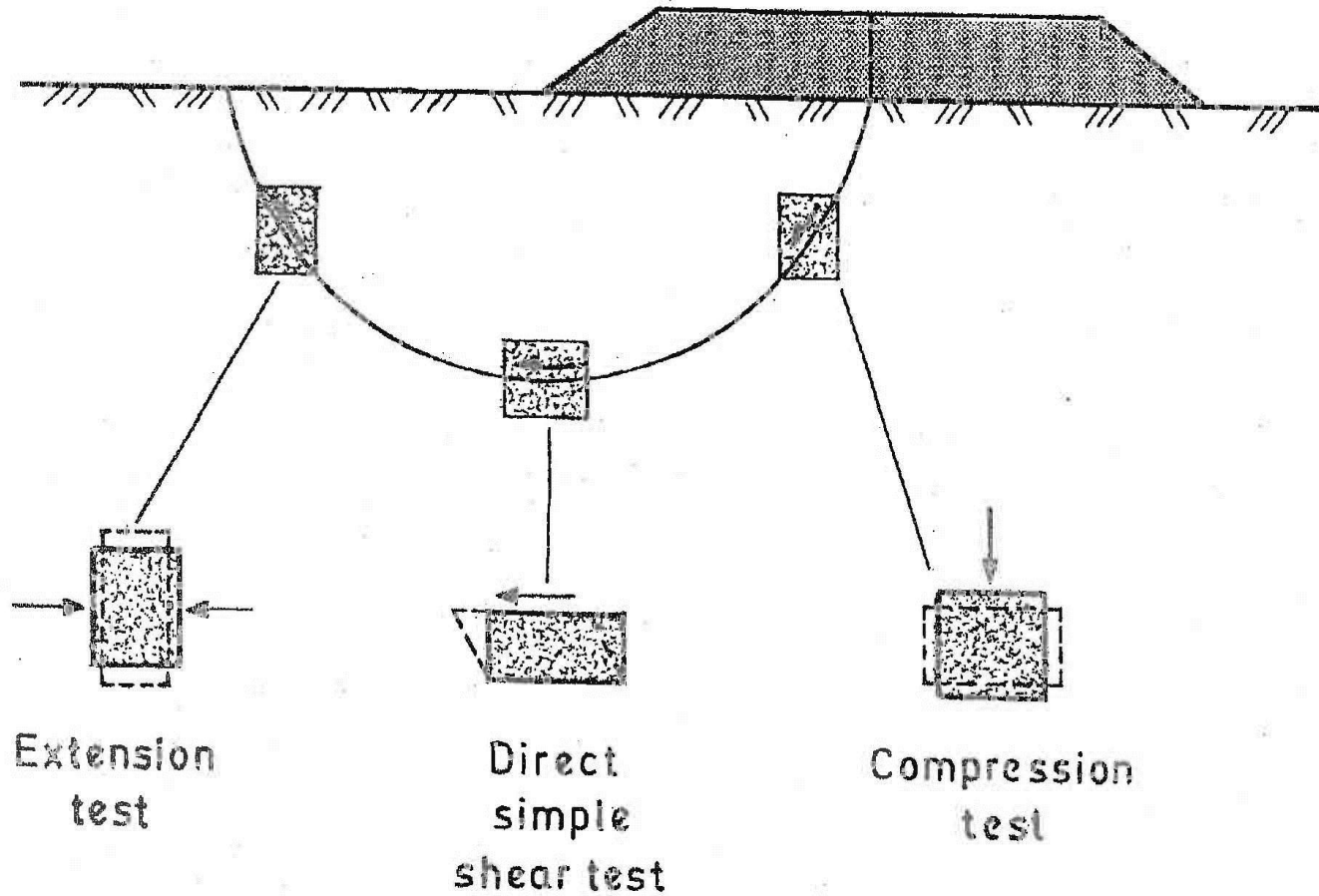


Fig. 1 Relevance of laboratory shear tests to shear strength in the field (Ref1).

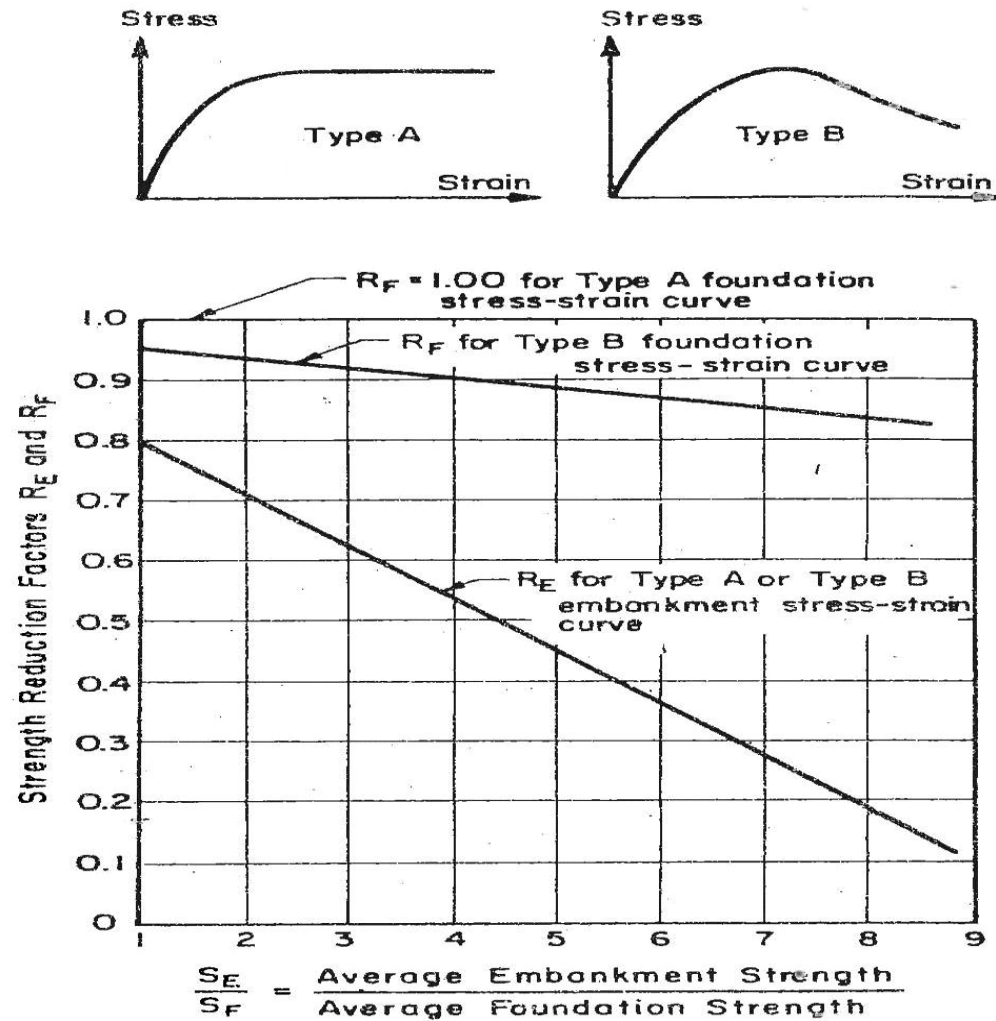


Fig. 2 CORRECTION FACTORS R_E AND R_F TO ACCOUNT FOR PROGRESSIVE FAILURE IN EMBANKMENTS ON SOFT CLAY FOUNDATIONS. (Ref.3)

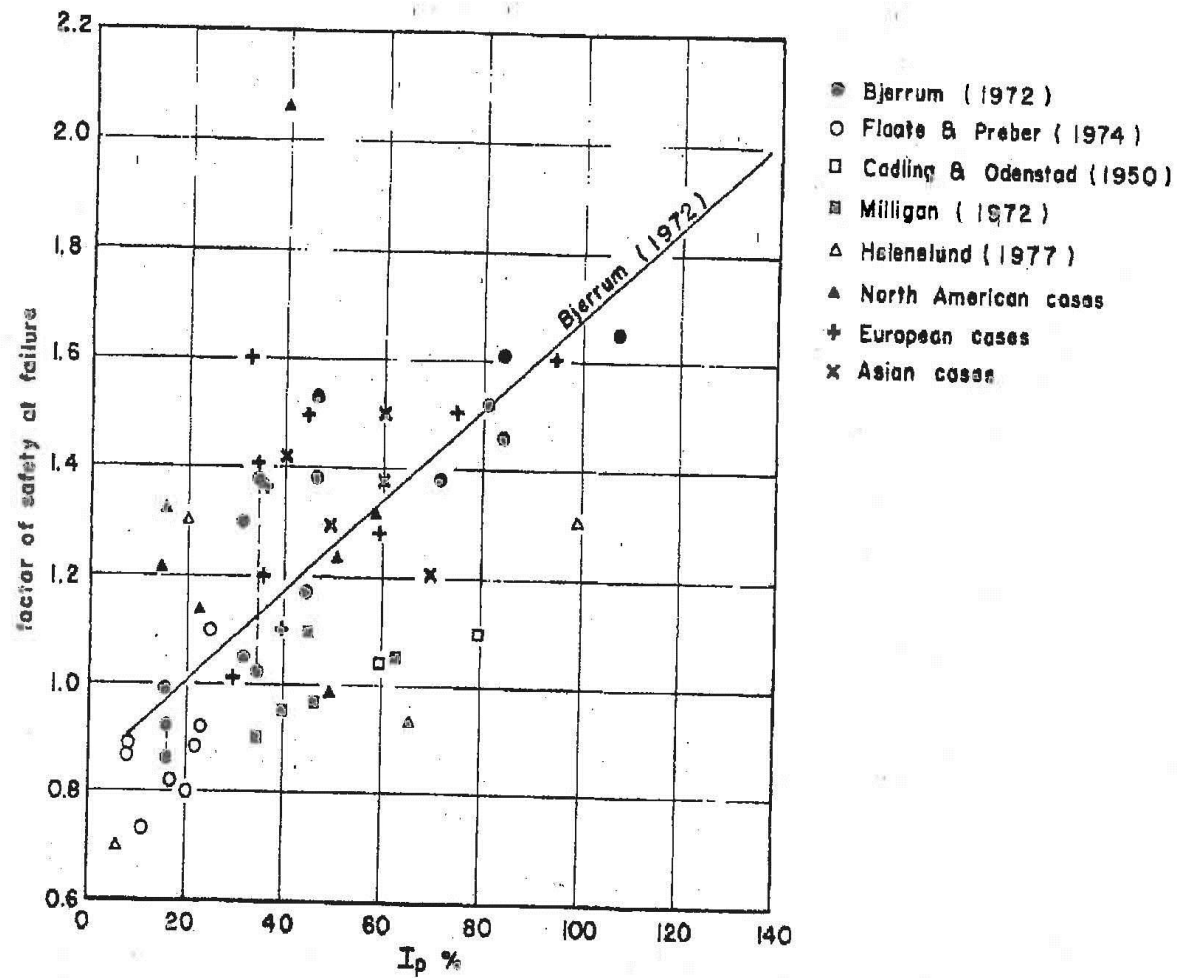


FIG. 3 Factors of safety at failure from all published case histories (as of 1979) (Ref 14).

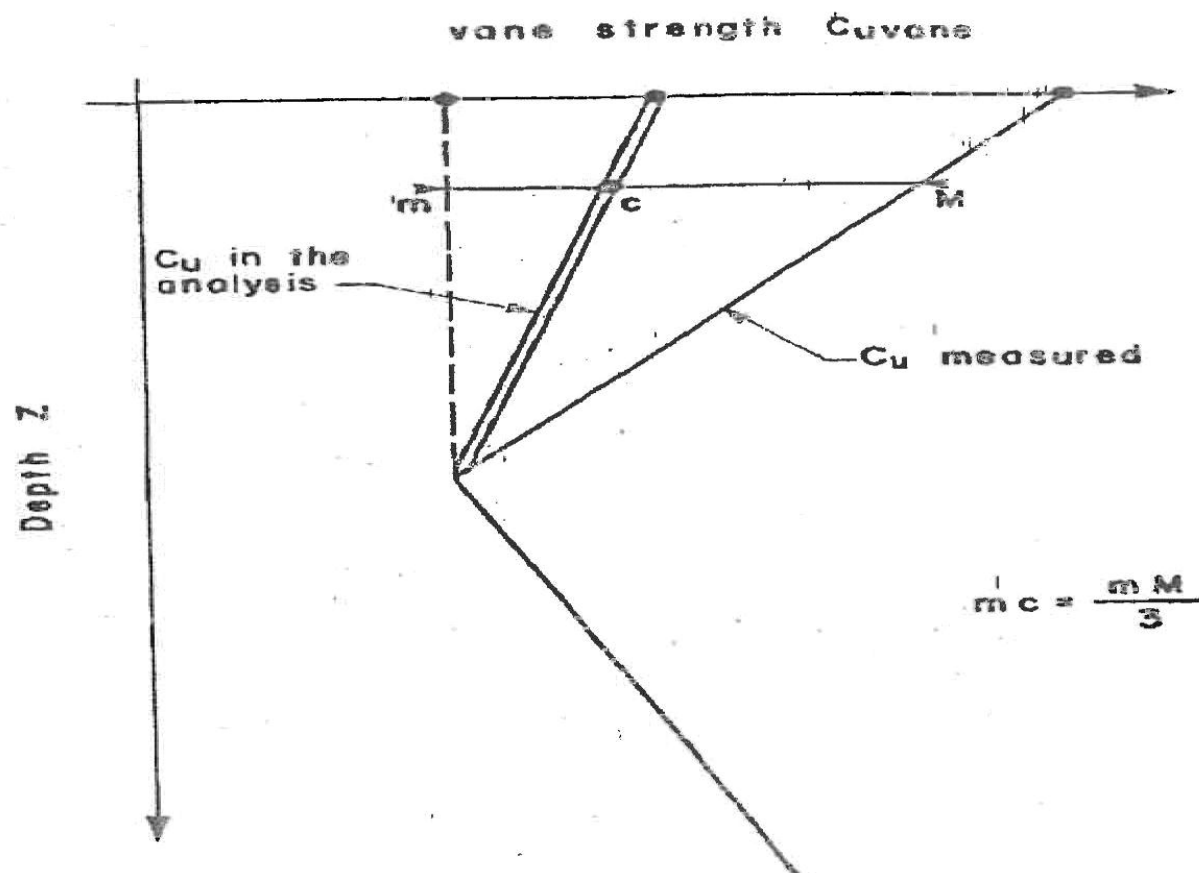


FIG. 4 . Strength profile in the weathered crust.
(REF 14)

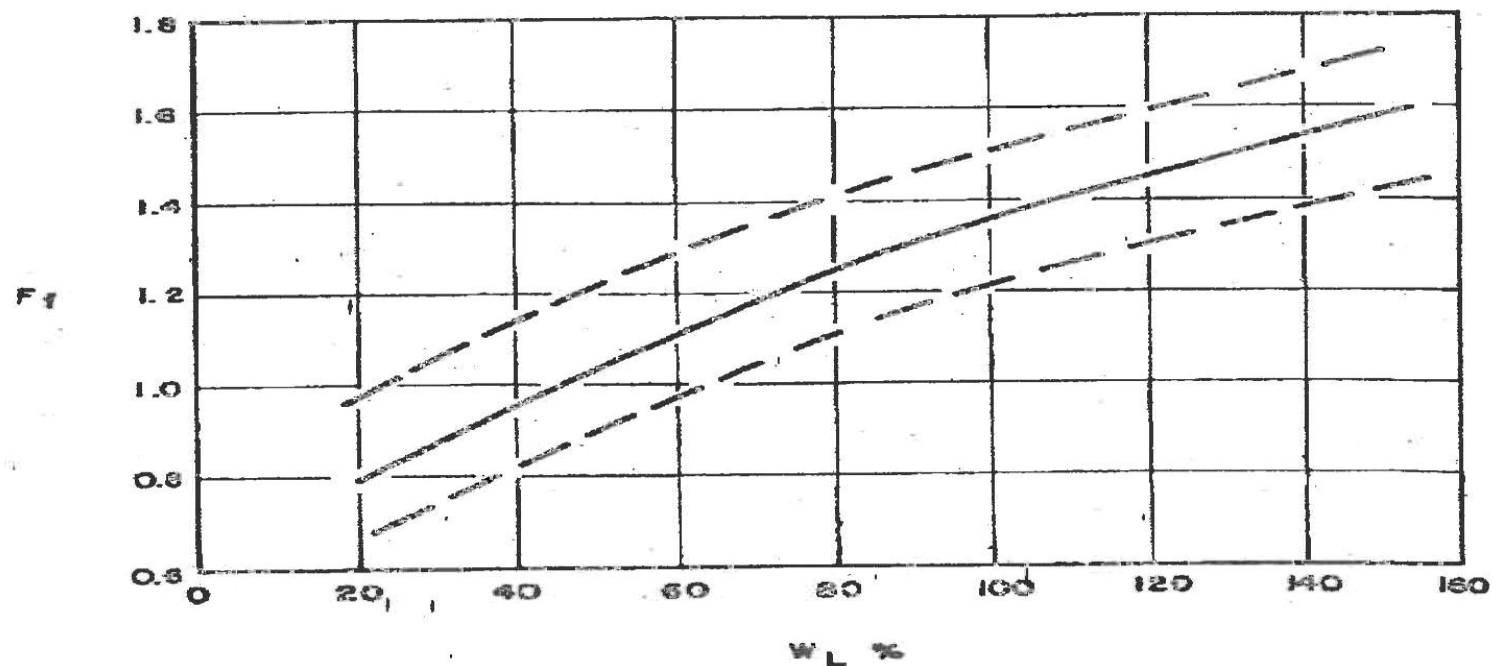
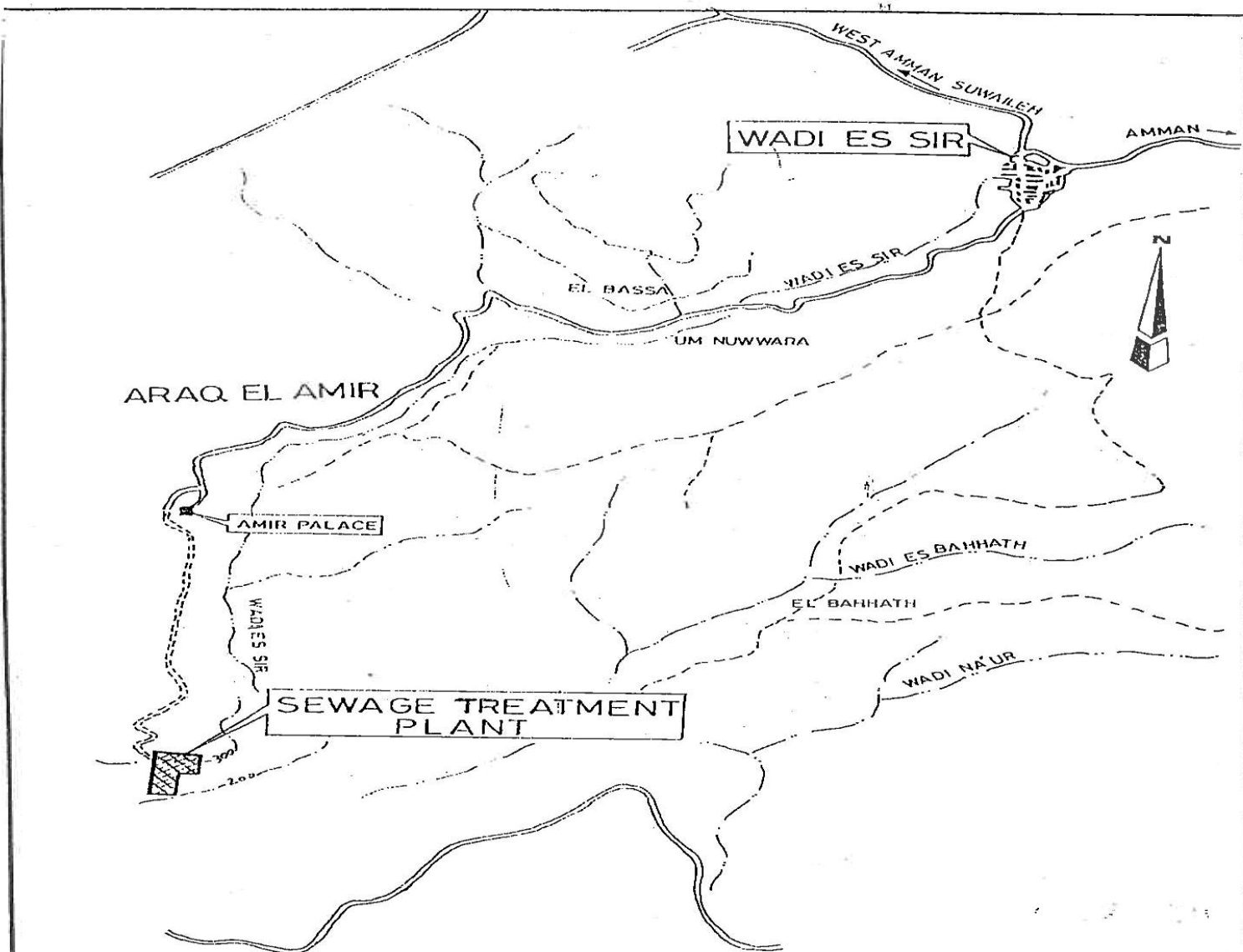


FIG. 5. Proposed correction of the factor of safety computed from the vane strength (Ref 14).



WADI ES SIR.
SEWAGE PROJECT

Fig. 6
GENERAL MAP

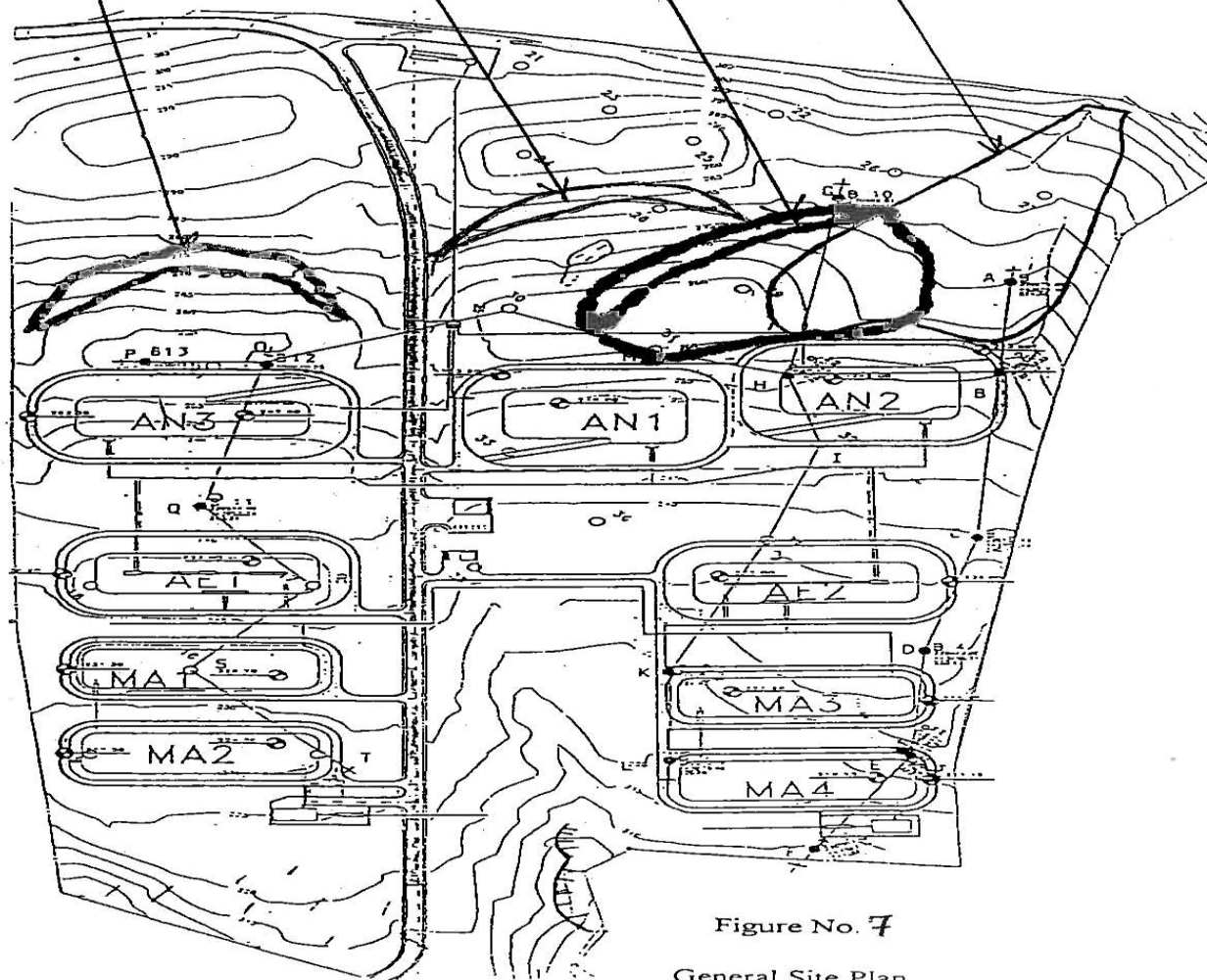


(1)
8 Sept., 1993
Landslide

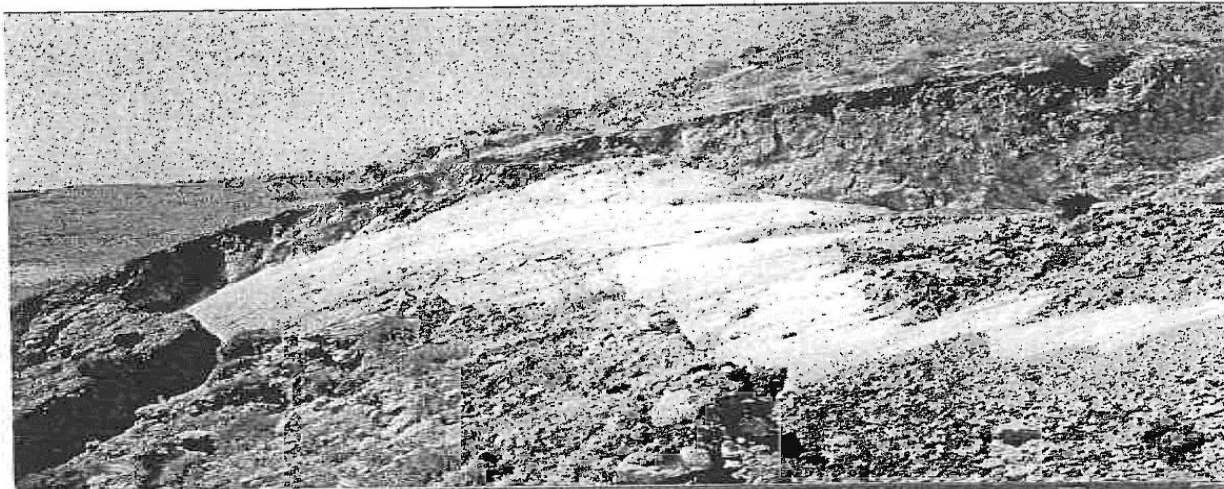
(2)
28 Nov., 1993
Landslide

(4)
23 Feb., 1997
Landslide

(3)
10 July, 1995
Landslide



(a)



(b)



Figure 8. July 10, 1995 landslide at WESTP project, (a) the 2 to 8m deep scarp with the sliding surface along the moderately dipping stratum of plastic clayey marl underlying the jointed weathered limestone, (b) the heave at the toe of the rotational slide in the plastic clayey marl.

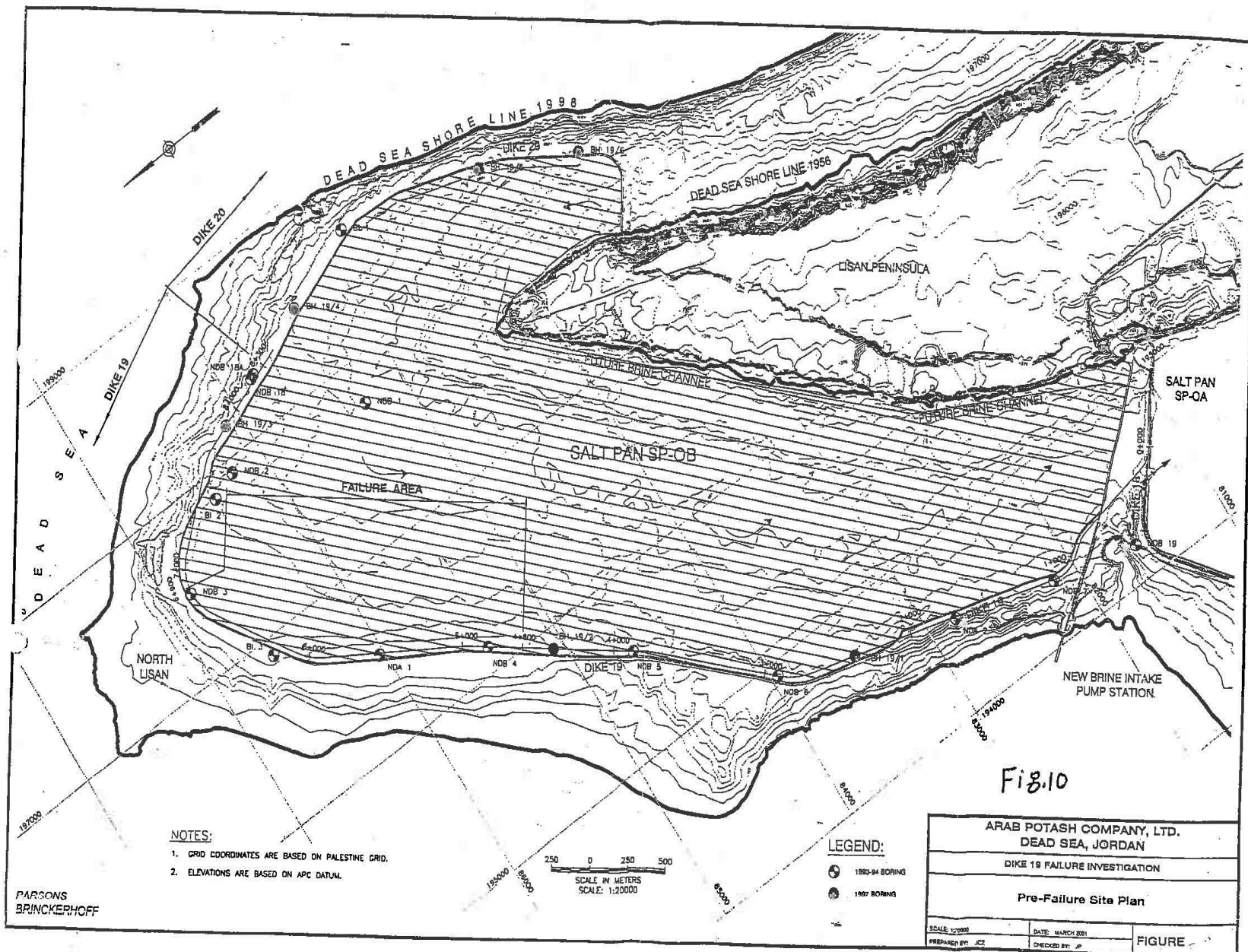
(a)



(b)



Figure 9. February 23, 1997 landslide at WESTP project, (a) the dislocation and separation of the gabion wall in the middle of the slide, (b) the standing undisturbed gabion adjacent to the displaced one with a dislocation of about 6 to 9m at the toe of the slide.



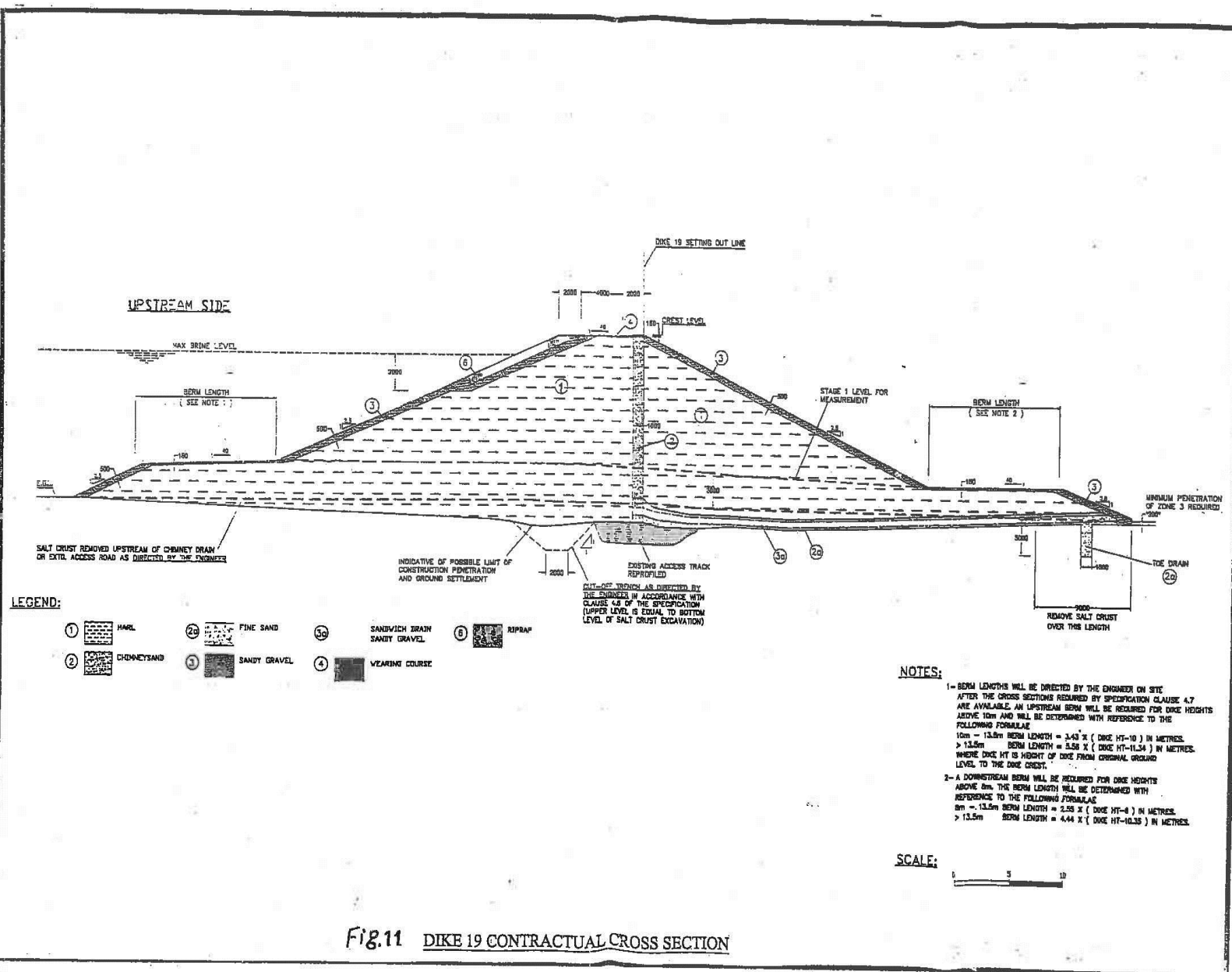


Fig.11 DIKE 19 CONTRACTUAL CROSS SECTION

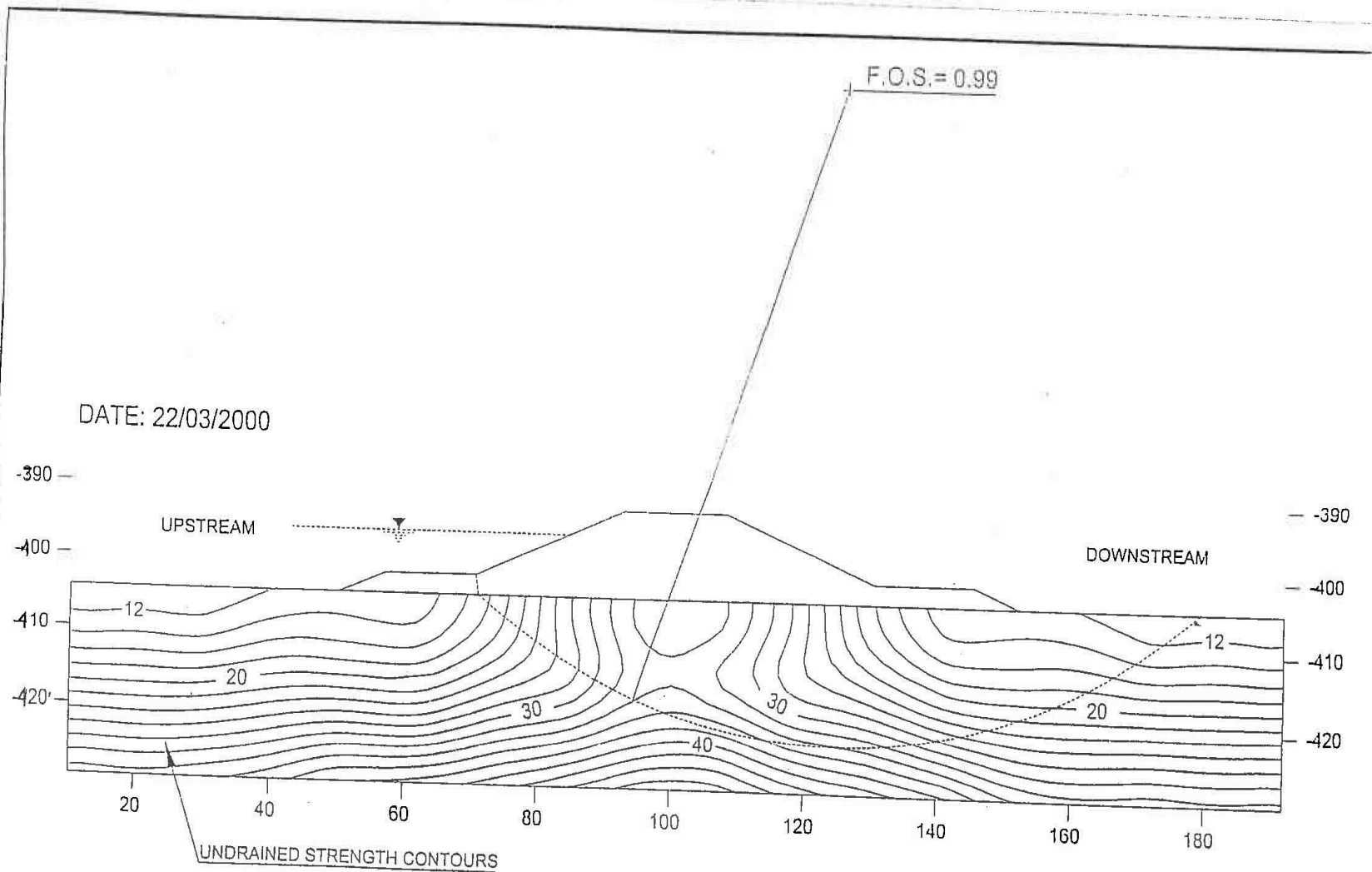


Fig. 12 END OF IMPOUNDMENT CRITICAL SLIP SURFACE (Ref. 2)



Not to Scale

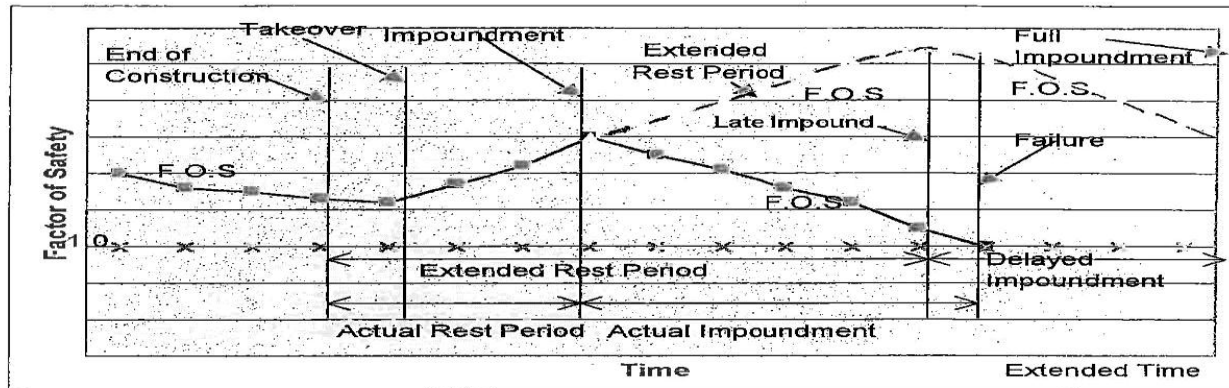


Fig. 13

An illustrative sketch that shows how the F.O.S. started to increase during the rest period and started to drop during impoundment until it reached 1.0 at time of failure. It also shows how an extended rest period and slower impoundment could have saved the dike with F.O.S. higher than 1.0 at full impoundment.